Application: AEF-A.17 Dynamic analysis of collision

KEY WORDS

Dynamic Analysis, Plane Geometric Model, Plane Stress State, Linear Material, 1D Finite Element, Linear Finite Element, Machine Element, Collision

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A. PROBLEM DESCRIPTION

A.1 Introduction

The Ansys Workbench Explicit dynamics suite it enables to capture the physics of shortduration events for products that undergo highly nonlinear, transient dynamic forces. In many cases, the accuracy of an explicit solution can be verified only via comparison with physical experiments. For some problems (such as explosions), it may be too expensive or impossible to perform tests.

"Implicit" and "Explicit" refer to two types of time integration methods used to perform dynamic simulations. Explicit time integration is more accurate and efficient for simulations involving – Shock wave propagation – Large deformations and strains – Non-linear material behaviour – Complex contact – Fragmentation – Nonlinear buckling.

Typical applications are drop tests, impact and penetration. ANSYS Explicit Dynamics analysis software provides simulation technology to help simulate structural performance long before manufacture.

A time integration method used in Explicit Dynamics analysis system. It is so named because the method calculates the response at the current time using explicit information. After defining the initial conditions (initial velocity, angular velocity), the analysis setting has to be maintained as per the problem requirement. In the analysis setting, time steps have to be defined explicitly, including:

- Initial time step
- Minimum time step
- Maximum time step
- Time step safety factor

In case of drop test the standard earth gravity is also taken into account.

ANSYS Explicit Dynamics utilizes the Autodyn solver within the standard ANSYS Mechanical interface to analyses transient structural events and it is used for simulating fracture, cutting, failure, buckling, impact, drop as well as highly nonlinear quasi-static simulations that the implicit APDL-based solvers would struggle to converge.



In practice, there are many mechanical phenomena that are manifested by mechanical contacts and stresses made in very short periods of time, in the form of collisions. Some of these collisions can cause elastic deformation of the parts in contact, others can cause plastic deformation or even destruction and expulsion of material (in the case of penetration phenomena). In the field of motor vehicles, these dynamic impact requirements are very common. An analysis of the impact phenomena between a body element and a static element is very suggestive, and can be used in the design stages of body elements and passive safety elements.



A.3 Application goal

The application aims to determine the maximum values of the fields of displacements, deformations, internal stresses produced in collision on the component elements.

For this analysis, the use of two-dimensional elements was considered due to the simplicity of the geometric construction and the ease of modifying the profile of the studied elements.

B. PREPARATION OF THE MODEL FOR ANALYSIS

B.1 The model definition

In order to draw up the finite element analysis model associated with the present application, it is necessary to identify:

- geometric shape and dimensions,
- restrictions induced by links with adjacent elements,
- external and internal loads (own weight, speeds, accelerations),
- material characteristics.

B.2 The analysis model description

The analyzed model is intended to be very simple, consisting of only two elements: one of the tubular type which represents a fixed obstacle (steel pipe pillar with an average diameter of 60 mm and the wall of 5 mm) and the other, of the panel type by alluminium alloy 1 mm thick sheet, representing the moving object (dimensions are presented in Chapter C.3 - Geometric modeling). The collision with the vertical pole is considered to take place in the normal direction of the sheet metal panel, in the middle of it, according to the drawing below. The metal pillar is embedded at the bottom and the sheet metal panel moves in the direction of Ox in the direction of approaching the pillar with a speed of 25 m / s.



- point A TX TY TZ RX RY RZ
- Vertical edges of the panel <mark>B</mark> TX RY
- $v_y = -25 \text{ m/s}$

B.3 Characteristics of the material

For finite element analysis the strength characteristics of the material, S235 steel are:

- modulus of longitudinal elasticity, $E = 204,000 \text{ N} / \text{mm}^2$;
- transverse contraction coefficient (Poisson), v = 0.3.

The characteristics of the second material, aluminum alloy, remain unchanged, according to the software library of materials.

- modulus of longitudinal elasticity, E = 75.000 N / mm²;
- transverse contraction coefficient (Poisson), v = 0.32.

C. PREPROCESSING OF FEA MODEL

C.1 Creating and saving the project
Create of the project
Λ , Toolbox : \Box Analysis Systems $\rightarrow \Box$ \Box Explicit Dynamics (the subproject window appears automatically); \rightarrow
[the name can be changed Explicit Dynamics în Collision].
<u>Problem type setting (3D)</u>
$A: \sqcup \widehat{\heartsuit} \text{ Geometry} \rightarrow \square \text{ Properties} \rightarrow \text{ Properties of Schematic A3: Geometry}, = Advanced Geometry Options}: \square \text{ Analysis Type},$
[select from list $ \downarrow \mathbf{Z}, \downarrow 3D$] \rightarrow [close window $\downarrow \mathbf{X}$].
Saving the project
$ \exists Save As \rightarrow \bigwedge Save As, File name: [input name, Collision] \rightarrow \exists Save As \rightarrow \bigwedge Save As, File name: [input name, Collision] \rightarrow \exists Save As \rightarrow \bigwedge Save As, File name: [input name, Collision] \rightarrow \exists Save As \rightarrow \bigwedge Save As, File name: [input name, Collision] \rightarrow \exists Save As \rightarrow \bigwedge Save As, File name: [input name, Collision] \rightarrow \exists Save As \rightarrow \bigwedge Save As, File name: [input name, Collision] \rightarrow \exists Save As \rightarrow \bigwedge Save As, File name: [input name, Collision] \rightarrow \exists Save As \rightarrow \bigwedge Save As, File name: [input name, Collision] \rightarrow \exists Save As \rightarrow \bigwedge Save As, File name: [input name, Collision] \rightarrow \exists Save As \rightarrow \bigwedge Save As, File name: [input name, Collision] \rightarrow \exists Save As \rightarrow \boxtimes Save A$
C.2 Modelling of material characteristics
As there will be two separate parts, two different materials will be considered: steel and aluminum.
Λ , Project Schematic: L, Sector Engineering Data \checkmark \rightarrow \rightarrow \checkmark Edit \rightarrow Outline of Schematic A2: Engineering Data



C.3 Geometric modelling
C.3.1 Loading DesignModeler (DM) module
$\land, Project Schematic: \Box & Geometry \rightarrow \Box \\ \land OK.$
C.3.2 Pillar modelling
Construct a pipe with a circular section along the OZ axis, with surface-type elements, as follows:
Tree Outline $\rightarrow \checkmark \checkmark \checkmark \land $
25 mm, 1000 mm long).
Dimensioning commands in the menu Dimensions will be used for sizing and positioning.
To create the 3D model, use the command Revolve, then rotate the drawn segment around the OZ axis, then

0.00	2000	
		C.3.3 Panel modelling
A rectangular panel is o	constructed in a plane	parallel to the XOZ, using surface-type elements. Since the panel
will have reinforcemen	ts on two edges its n	rofile will be drawn in a plane perpendicular to the 07 and XOY
	ts on two edges, its p	to the will be drawn in a plane perpendicular to the OZ and XOT
axis, respectively.		
Tree Outline	XYPlane Skatching	
	\rightarrow <u>sketching</u>	(draw the profile in the figure
below).		
* 1		
- 114		
1 10		, , , , , , , , , , , , , , , , , , , ,
		u
		T •
	H1 300 mm	
	L3 70 mm	Ma Jife
	L4 40 mm	Nidily
	L5 40 mm	Hadius: 15 mm
The profile will be extr	uded with the 💽 Extru	de command in the OZ direction on the length of 400 mm then
it will be translated in the	$h_{0} OZ$ direction at he	If the height of the noise respectively 200 mm using the
	Ine OZ uncetion at has	in the height of the pole, respectively 500 min, using the
commands:		
Create Body Transf	\bullet ormation \bullet \rightarrow	${}_{\blacksquare}$ Translate \rightarrow \neq Generate
Tree Outline		A. A.
C: Geometry		
TXPlane		
YZPlane		
E Revolve5		
Extrude2		Y
Translate1		1
Pillar		
Panel		0.00 150.00 j00.00 (mm)

C.3.4 Saving the geometric model
$\textcircled{0} \rightarrow \blacksquare$ (Save Project) $\rightarrow \underline{File} \rightarrow Close$ Design Modeler.
C.4 Finite element modelling
C.4.1 Activate the discretization module and set the finite element type
Launching of the finite element modeling module
N, Project Schematic \rightarrow launching module Mechanical [ANSYS Multiphysics].
Setting the unit of measurement system
Units $\rightarrow \downarrow$ Metric (mm, kg, N, s, mV, mA) (the system of units of measurement is usually set by default).
$\underbrace{\text{Outline}}_{: \downarrow} \bigoplus \underbrace{\text{Geometry}}_{: \downarrow} \bigoplus \underbrace{\text{Geometry}}_{: \downarrow} \bigoplus \underbrace{\text{Pillar}}_{: \downarrow} Assignment}_{: \downarrow} Assignment} \rightarrow \underbrace{\text{Select from list}}_{: \downarrow} \bigoplus \underbrace{\text{Geometry}}_{: \coprod} \bigoplus \underbrace{\text{Geometry}}_{: \bigoplus} \bigoplus \underbrace{\text{Geometry}}_{: \bigoplus} \bigoplus \underbrace{\text{Geometry}}_{: \coprod} \bigoplus \underbrace{\text{Geometry}}_{: \bigoplus} \bigoplus \text{Geom$
Structural Steel (default)] \rightarrow Definition \rightarrow Thickness 4.e-003 m
$\underbrace{Outline}_{:} \ \ \square \xrightarrow{\bullet} \ \ \square \ \ \square \ \ \square \ \ \square \ \square \ \square \ \square \ \ \square \ \ \square \ \square \ \square$
$ \exists \text{Aluminum Alloy} (default)] \rightarrow \overset{\text{Definition}}{\rightarrow} \overset{\text{Thickness}}{\rightarrow} 1.e-003 \text{ m} . $
C.4.2 Model discretization and finite element size setting
\bigcirc Outline : \rightarrow Mesh \rightarrow Sizing \bigcirc \rightarrow Details of "Edge Sizing" - Sizing \rightarrow Scope \rightarrow Select Geometry: [will
be selected with .13D geometry of the pillar using the selection filter (Body) Apply: Definition Element
50 Selected with 2 55 geometry of the print, using the selection riter (5003)] rippiy, 50 million 210 metric
\rightarrow Size: 10 mm \rightarrow Update \sim .
The operation will be repeated for the other body as well - Panel, Size: 10 mm.
C.5 Modeling joints and constraints
Inserting the fixed support
$\bigcirc \text{Outline} : \neg \mathbb{R} \text{ Explicit Dynamics} \downarrow \bigcirc \text{Fixed} \rightarrow \text{Details of "Fixed Support"} \rightarrow \text{Geometry} \rightarrow \text{Scope: [the circle]} $
at level 0 corresponding to the pillar is selected using the selection filter 🛅 (Edge)].
Details of "Fixed Support"
Scoping Method Geometry Selection
Geometry 1 Edge
- Definition
Type Fixed Support
Suppressed No



D. SOLVING THE FEA MODEL





E. POST-PROCESSING OF RESULTS

E.1 Viewing the displacement fields
For suggestive results, set the view scale of the menu bars:
Result 8,6e+002 (Auto Scale) ▼ → Result 1.0 (True Scale) ▼
Total deformation view
\downarrow \sim Solution (A6) \rightarrow \sim \sim Total Deformation \rightarrow Graph \rightarrow Animation \triangleright
If the images are not suggestive enough, in terms of how the work is distorted, you can return to changing the
display scale by selecting a higher value: Result 1,7e+003 (2x Auto)
Various forms of distorted state representation can be used by calling the 💋 - (Edge) button. Show
Showformed WireFrame will be selected, an option that displays the undeformed and warped models in the same representation.
Image:
The display characteristics can be changed: the number of frames ^{10 Frames} , as well as the running
time of the simulation. At the same time, the result can be saved as a video file using the Export Video File
command 🍱.
Total deformation view
$ \exists for a constant for a constant of the second s$
D: Explicit Dynamics Total Deformation Type: Total Deformation Unit m Time: 55009-003 s Cycle Number: 4847 02/12/22 12:39 PM 0.17881 Max 0.15894 0.13908 0.11921 0.099339 0.079472 0.059604 0.039736 0.019968 0 Min
If you want to view it in another direction, follow the steps below:
\rightarrow Details of "Directional Deformation" \rightarrow Details of "Directional Deformation" \rightarrow Definition \rightarrow Orientation
\checkmark : Y Axis \rightarrow $\stackrel{\Rightarrow}{\rightarrow}$ Solve



Tal	bular Data				- ‡ □ ×
Tal	bular Data Time [s]	Force Reaction (X) [N]	Force Reaction (Y) [N]	Force Reaction (Z) [N]	
Tal	bular Data Time [s] 6.0003e-003	Force Reaction (X) [N]	Force Reaction (Y) [N] 2307.3	Force Reaction (Z) [N]	✓
Tal 13	bular Data Time [s] 6.0003e-003 6.5007e-003	Force Reaction (X) [N] -328.63 464.37	Force Reaction (Y) [N] 2307.3 5059.5	Force Reaction (Z) [N] 659.87 -4897.5	
Tal 13 14 15	bular Data Time [s] 6.0003e-003 6.5007e-003 7.001e-003	Force Reaction (X) [N] -328.63 464.37 335.72	Force Reaction (Y) [N] 2307.3 5059.5 6727.6	Force Reaction (Z) [N] 659.87 -4897.5 -1172.2	 ↓ ↓ ↓ ✓ Force Reaction (Total) ∧ 2422.2 7056.9 6837.2
Tal 13 14 15 16	bular Data Time [s] 6.0003e-003 6.5007e-003 7.001e-003 7.5002e-003	Force Reaction (X) [N] -328.63 464.37 335.72 -461.69	Force Reaction (Y) [N] 2307.3 5059.5 6727.6 2355.4	Force Reaction (Z) [N] 659.87 -4897.5 -1172.2 -606.84	 ↓ □ × Force Reaction (Total) ∧ 2422.2 7056.9 6837.2 2475.8
Tal 13 14 15 16 17	bular Data Time [s] 6.0003e-003 6.5007e-003 7.001e-003 7.5002e-003 8.0005e-003	 ✓ Force Reaction (X) [N] -328.63 464.37 335.72 -461.69 417.92 	Force Reaction (Y) [N] 2307.3 5059.5 6727.6 2355.4 483.06	Force Reaction (Z) [N] 659.87 -4897.5 -1172.2 -606.84 2291.	 ↓ ↓ ↓ ✓ Force Reaction (Total) 2422.2 7056.9 6837.2 2475.8 2378.3
Tal 13 14 15 16 17 18	Construction Construction Time [s] 6.0003e-003 6.5007e-003 7.001e-003 7.001e-003 7.5002e-003 8.0005e-003 8.5008e-003	 ✓ Force Reaction (X) [N] -328.63 464.37 335.72 -461.69 417.92 -43.553 	Force Reaction (Y) [N] 2307.3 5059.5 6727.6 2355.4 483.06 1236.6	Force Reaction (Z) [N] 659.87 -4897.5 -1172.2 -606.84 2291. 2040.5	 ↓ □ × Force Reaction (Total) ∧ 2422.2 7056.9 6837.2 2475.8 2378.3 2386.4
Tal 13 14 15 16 17 18 19	Filter Filter<	Force Reaction (X) [N] -328.63 464.37 335.72 -461.69 417.92 -43.553 -803.21	Force Reaction (Y) [N] 2307.3 5059.5 6727.6 2355.4 483.06 1236.6 -326.26	Force Reaction (Z) [N] 659.87 -4897.5 -1172.2 -606.84 2291. 2040.5 -1053.	 ♀ ♀ □ × ¥ □ × ¥ □ × ¥ □ × ¥ ↓ ↓ ↓ ↓ ↓ ↓ ↓ ↓ ↓ ↓

F. RESULTS ANALYSIS

It is observed that, despite the fact that the modeling of the parts was performed with the help of surface type bodies, the results obtained are suggestive, being presented in a 3D environment, due to the ease of the program used to attach various thicknesses to the structure.

Changing the thickness and materials of the various components is very easy to do, this can be done even at the end of an analysis, and after an update order, the results of the new analysis will change according to the new initial conditions.

From the point of view of the total deformations, it is observed that the maximum value is 0.0175 m in the area of the vertical edges, the entities furthest from the center of the panel.

Examining the graphical representation of the total equivalent stresses (fig.a), it is observed that the panel is strongly stressed in the areas of contact with the column, reaching values (543 MPa) that exceed the elastic limit of the material, entering the flow area ($\sigma_c=280$ Mpa).

In other words, at these initial data (constraints and speed of the panel) a plastic deformation of the panel can be noticed.

From the point of view of the tubular pillar, made of steel (fig. b), a voltage of values of 180-200 Mpa is observed, below the flow limit. So, the pillar will deform elastically, returning to its original shape and dimensions.

If the initial speed changes from 25 to 10 m/s, it will be noticed that the value of the stresses generated by the impact is lower (280 Mpa), as well as the deformation of the panel (0.005 m), remaining in the area of elastic deformations.



G. CONCLUSIONS

From the point of view of the pre-processing phase, it can be seen that the use of 2D bodies involves minimal resources for both modeling and discretization. Another strong point is that the thickness of the parts (either of the column or of the sheet metal panel) can be modified very easily, without influencing the basic shape of the bar structure.

The introduction of supports, constraints and demands is quick and easy. The declaration of materials, as well as the discretization of the structure in the form of surfaces are controllable processes, and can be done automatically or manually.

Analyzing the results obtained by FEM, it can be seen that it provides much more data, at a time and with much lower resource consumption, than the analytical version.