Application: AEF-A.16

Static analysis of bar mechanisms

KEY WORDS

Linear Static Analysis, Plane Geometric Model, Plane Voltage State, Linear Material, 1D Finite Element, Linear Finite Element, Machine Element, Mechanical Subassembly, Bar Mechanisms, Joints

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A. PROBLEM DESCRIPTION

A.1 Introduction

In various finite element analysis (FEA) applications it is necessary to model not only a single part, but also a whole mechanism, including the joints between its elements.

Complex plane or spatial mechanisms can be reduced to bar mechanisms (levers) and toothed mechanisms (gears and racks). The methods of studying the complex mechanisms with bars and gears are very diverse, especially in the field of kinematics, starting from the hypothesis of the rigidity of the components. This paper aims to study the behavior of the elements of a bar mechanism, taking into account their elastic behavior.

A.2 Application description

From a constructive point of view, the jack in the figure below is a flat mechanism consisting of four bars of various sections mounted on a support, a screw and a nut that make a helical coupling. The analyzed jack can operate within two positions: A - start lifting and B - maximum lifting.

The vertical movement of the upper plate 5 is determined by the change of the positions of the side segments 2, mounted by means of support joints 1, due to the axial movement of the nut 6. The screw 3 is actuated by means of the crank 4.

All the joints between the segments 2 and the support 1, between the segments 2 and the upper plate 5, as well as those between the lower and the upper segments are flat rotational couplings.

By rotating the crank 4, thanks to the nut 6, the side segments of the jack tend to approach each other, generating vertical movement, thus lifting the vehicle.



stresses produced in operation on the component elements. For this analysis, the use of one-dimensional elements was considered due to the simplicity of the geometric construction, the ease of modifying the profile of the studied elements but also the main objective - to use the joints in the study with finite elements.

B. PREPARATION OF THE MODEL FOR ANALYSIS

B.1 The model definition

In order to draw up the finite element analysis model associated with the present application, it is necessary to identify:

- geometric shape and dimensions,
- restrictions induced by links with adjacent elements,
- external and internal loads (own weight),
- material characteristics.

B.2 The analysis model description

The dimensions of the studied mechanism, respectively the lengths of the segments and their sections, are presented in chapter C.3.2, C.3.3 and C.3.4, these being, on the one hand, taken from the specialized literature and, on the other hand, imposed from constructively so that the problem is determined.

The construction of the segments 2, of the vertical zones afferent to the guide bush (7) and the nut 6, the upper plate 5 are constructed in the form of one-dimensional bars.

The connections between these bars are made with simple rotating joints (CR in the adjacent drawing). In addition, the vertical side segments will have translational movements only in the plane of the mechanism, without rotations.

The external loads, generated by the mass of the raised vehicle, are shaped by the rigid fixing of the support 1 and the upper plate 5, and the forces generated by the screw act on the horizontal axis, on the lateral vertical segments, in the direction of approaching the lateral segments.



• transverse contraction coefficient (Poisson), v = 0.3.

C. PREPROCESSING OF FEA MODEL



Propertie	es of Outline Row 3: Structural Steel			•	-12	×
	А	В	С	D	Е	
1	Property	Value	Unit	8	ĠΖ	
2	🔁 Density	7850	kg m^-3 🔹 💌			
3	■ Bisotropic Secant Coefficient of Thermal Expansion					
6	🗉 🛛 Isotropic Elasticity					
7	Derive from	Young's 💌				
8	Young's Modulus	2E+11	Pa 🔹			
9	Poisson's Ratio	0,3				
10	Bulk Modulus	1,6667E+11	Pa			
11	Shear Modulus	7,6923E+10	Pa			
12	🗉 📔 Alternating Stress Mean Stress Shear M	lodulus abular				
16	🗉 🔁 Strain-Life Parameters					
24	🔁 Tensile Yield Strength	2,5E+08	Pa 🔹			Ţ
			· · · ·			_











acceleration implies the taking into account of the own weight of the metallic structure) \rightarrow Details of "Standard Earth Gravity" \rightarrow Definition \rightarrow Direction \checkmark : -Y Direction.

Insertion of the base connection joints

 Θ , Outline : $\Box = \sqrt{2}$ Connections $\to = 2$ Body-Ground $\bullet \to 0$ Revolute \to Details of "Revolute - Ground To No Selection" $\to 0$

Mobile \rightarrow Scope: [select Point 1 using the selection filter 1 (Point)]. A rotating joint around the Oz axis is being considered

De	etails of "Revolute - G	round To No Selection"	
-	Definition		
	Connection Type	Body-Ground	
	Туре	Revolute	
	Torsional Stiffness	0, N·mm/°	Developer Crewed To She inf
	Torsional Damping	0, N'mm's/°	20.01.2015.19:41
	Suppressed	No	20.01.2013 19.41
	Reference		□ ×
	Coordinate System	Reference Coordinate System	
	Mobile		
	Scoping Method	Geometry Selection	
	Scope	No Selection	
	Body	No Selection	
	Initial Position	Unchanged	RZ

The operation will also be repeated for Item 8, in connection with the base.

Insertion of	^c joints	between	segments	
			-	

Reference \rightarrow Scope: [Point 2 on the Dr_inf segment is selected using the selection filter (Point)] \rightarrow **Apply** \rightarrow **Mobile** \rightarrow Scope: [the same Point 2 is selected, but which is located on the Dr_med segment, using the selection filter (Point)] \rightarrow **Apply**.

🖸 Outline · 🔄 ""🖓 Connections 🛶 🗞 Body-Body 🗸 🛶 💠 Revolute 🛶 Details of "Revolute - No Selection To No Selection"

When selecting the same point, the symbol below will appear in the lower left corner of the graphic window, which is the command button to toggle the selection of the two entities (segments, in this case) by clicking with the mouse on the two planes.



Details of "Revolute - No Selection To No Selection"			De	Details of "Revolute - Dr_inf To Dr_med"			
	Torsional Damping	0, N'mm's/°		Torsional Damping	0, N·mm·s/°		
	Suppressed	No		Suppressed	No		
-	Reference		E	Reference			
	Scoping Method	Geometry Selection		Scoping Method	Geometry Selection		
	Scope	No Selection		Scope	1 Vertex		
	Body	No Selection		Body	Dr_inf		
	Coordinate System	Reference Coordinate System		Coordinate System	Reference Coordinate System		
	Behavior	Rigid		Behavior	Rigid		
	Pinball Region	All		Pinball Region	All		
-	Mobile		E	Mobile			
	Scoping Method	Geometry Selection		Scoping Method	Geometry Selection		
	Scope	No Selection		Scope	1 Vertex		
	Body	No Selection		Body	Dr_med		
	Initial Position	Unchanged		Initial Position	Unchanged		
	Behavior	Rigid		Behavior	Rigid		
					1		

Repeat the operation for the other torques in points 3, 4, 5, 6, 7 and obtain the torques shown in the tree below.



Introduction of operating constraints

The jack will work taking into account the hypothesis that the median lateral segments will be able to move only in the xOy plane, without the possibility to rotate.





D. SOLVING THE FEA MODEL

D.1 Launching the calculation module and select the types of results

In order to select the final data types to be analyzed after the launch of the calculation module, the series of commands presented below will be followed.



E. POST-PROCESSING OF RESULTS

E.1 Viewing the displacement fields
For suggestive results, set the view scale of the menu bars:
Result 8,6e+002 (Auto Scale) \checkmark \rightarrow Result 1.0 (True Scale) \checkmark
Total deformation view
\rightarrow " $\sqrt{29}$ Solution (A6) \rightarrow $\sqrt{49}$ Total Deformation \rightarrow Graph \rightarrow Animation \blacktriangleright
If the images are not suggestive enough, in terms of how the work is distorted, you can return to changing the
display scale by selecting a higher value: Result 1,7e+003 (2x Auto)
Various forms of distorted state representation can be used by calling the 27 (Edge) button. Show
Showformed WireFrame will be selected, an option that displays the undeformed and warped models in the
same representation.
(2) Probe
WireFrame
🔞 Show Undeformed Model
🔕 Show Elements



E.2. Visualize the fields of stress, forces and moments





F. RESULTS ANALYSIS

It is observed that, despite the fact that the modeling of the articulated bar mechanism was performed with the help of one-dimensional bodies, the results obtained are suggestive, being presented in a 3D environment, due to the ease of the program used to attach various profiles to the structure. executed by the user. Modifying the profiles of the articulated bars is very easy to do, this can be done even at the end of an analysis, following that after an update command, the results of the new analysis will change according to the new initial conditions.

The realization of the rotational torques is easy, it is not necessary their 3D construction and the precise modeling of their geometry. The definition of the rotational torques can take into account the elastic characteristics of the joint. The positioning of the torques according to the bar profile can be chosen from several variants, offered by ANSYS.

From the point of view of the total deformations, it is observed that the maximum value is 0.05 mm in the area of application of the stress, in the direction of the Ox axis.

Examining the graphical representation of the axial stresses, it is observed that the lateral segments (2) are subjected to the compression stress - represented in blue. The information regarding the deformations, corroborated with the information regarding the internal stresses, the combined maximum stresses lead to the conclusion that the structure withstands loads without problems, the values of the maximum stresses not exceeding the allowed material limit (compression $\sigma_{ac}=80$... 100 Mpa).

Definition				
Connection Type	Body-Ground			
Туре	Revolute			
Torsional Stiffness	0, N·mm/°			
Torsional Damping	0, N·mm·s/°			
Suppressed	No			
Reference	·			
Coordinate System	Reference Coordinate System			
Mobile				
Scoping Method	Geometry Selection			
Scope	1 Vertex			
Body	Inf_stg			
Initial Position	Unchanged			
Behavior	Rigid 💌			
Pinball Region	Rigid			
Stops	Deformable Beam (Beta)			

G. CONCLUSIONS

From the point of view of the pre-processing phase, it can be seen that the use of 1D bodies involves minimal resources for both modeling and discretization. Another strong point is that the transverse profile of the sections can be modified / oriented very easily, without influencing the basic shape of the bar structure. Moreover, it is possible to use different profiles for each section. The sections can be connected in several ways, depending on the central axis of the profiles used.

The introduction of supports, constraints and demands is quick and easy. The declaration of the materials, as well as the discretization of the bar structure are controllable processes, which can be done automatically or manually.

Analyzing the results obtained by MEF, it can be seen that it provides much more data, at a time and with much lower resource consumption, than the analytical version. It can be seen that the structure of the beams is very little required, and smaller profiles can be used in order to achieve savings. Changing the profile of the beam sections and recalculating is done in a very short time, being an easy procedure.